



Estimation of Modulus of Elasticity in Static Bending of Wood in Structural Dimensions as a Function of Longitudinal Vibration and Density

**Raquel Schmitt Cavalheiro¹, Diego Henrique de Almeida^{2*},
Tiago Hendrigo de Almeida¹, André Luis Christoforo²
and Francisco Antonio Rocco Lahr³**

¹*Department of Science and Materials Engineering, University of São Paulo, Av. Trabalhador São-Carlense 400, São Carlos - SP, 13566-590, Brazil.*

²*Department of Civil Engineering, Federal University of São Carlos, Rodovia Washington Luís, km 235 - SP310, São Carlos - SP, 13565-905, Brazil.*

³*Department of Structures, University of São Paulo, Av. Trabalhador São-Carlense 400, São Carlos - SP, 13566-590, Brazil.*

Authors' contributions

This work was carried out in collaboration between all authors. Authors RSC and FARL designed the study, wrote the protocol and managed the analyses of the study. Author ALC wrote the protocol and statistical analysis. Authors DHA and THA managed the analyses of the study, wrote the first draft of the manuscript and managed the literature searches. All authors read and approved the final manuscript

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ABSTRACT

In order to use wood in a sustainable and rational way, it is necessary to estimate its characteristics, and in the case of civil construction, the physical and mechanical properties are the most interesting. The aim of this research was to estimate the modulus of elasticity of structural pieces of

*Corresponding author: E-mail: diegoestruturas@gmail.com;

Schizolobium amazonicum Herb. wood through static bending (MOE_{sb}) and longitudinal vibration (MOE_{lv}) methods, in addition, to generate regression models to estimate the modulus of elasticity of static bending. Tests for MOE_{sb} and MOE_{lv} estimation were carried out according to ABNT NBR 7190:1997 and FAKOPP Enterprise, respectively. Linear and quadratic regression models were used to estimate MOE_{sb} as a function of MOE_{lv} . A multivariate regression model was also generated considering the wood density. According to the discussion of the obtained results, MOE_{lv} and MOE_{sb} average values estimated for the studied batch of *Schizolobium amazonicum* Herb. wood were 9.70 and 9.07 GPa, and average density 381.21 kg/m³. Regression models proposed for estimation of MOE_{sb} presented the coefficient of determination close to 60%.

Keywords: Mechanical properties; modulus of elasticity; wood; wood structures.

1. INTRODUCTION

Wood is one of the main raw materials used throughout the world, from different types of tools used in agriculture and animal husbandry practices [1], to artifacts with greater added value [2] reaching advanced technological and constructive aspects [3].

This diversity of wood uses is due to the ease of obtaining and processing of this material [4,5]. Brazil is one of the main countries in the world in relation to the forest sector, since it has a certified forest area equal to 6,378,006 ha [6], in its different biomes, each with specific characteristics of the flora [7,8], among they are the Amazon Forest.

There is no consensus among the exact number of tree species that are in the Amazon Forest [9], recent research estimates that 16,000 species [10], many of them not yet cataloged, without knowledge of their properties and technological potential. However, the scientific community has been developing research to determine the properties of natural resistance to the xylophagous organisms attack [11], physical and mechanical [12,13] and chemical properties [14]. Besides, due to the extension of the Amazon Forest region, edaphoclimatic factors [15] should be considered for determination of wood properties [16,17].

Among the species of trees coming from the Amazon Forest, the *Schizolobium amazonicum* Herb. (common name: Paricá) stands out, due to its rapid growth [18], physical and mechanical properties that allow its use in civil construction, either as a structural element [19] or in glulam manufacturing [20].

In order to use wood in construction, it is necessary to determine its physical and

mechanical properties [21,22] according to specific Standard Codes, such as Brazilian [23] and European [24]. However, when it is impossible to produce specimens [25] or pieces present structural dimensions [26], non-destructive tests are performed by different techniques, including transverse vibration [27,28], acoustic tomography [29] and ultrasound [30]. In addition, it is also possible to estimate wood properties as a function of other known properties using regression models [31-34].

This research aims to estimate the modulus of elasticity of structural pieces of *Schizolobium amazonicum* Herb. wood through static bending and longitudinal vibration methods, in addition, to generate regression models to estimate the modulus of elasticity in static bending.

2. MATERIALS AND METHODS

Experimental procedures were performed at the Wood and Timber Structures Laboratory (LaMEM), at the School of Engineering of São Carlos (EESC), University of São Paulo (USP), in the city of Sao Carlos, São Paulo, Brazil.

2.1 Selection and Preparation of Test Specimens

Pieces presenting structural dimensions (boards) of a batch of *Schizolobium amazonicum* Herb. wood from a certified area in the northern region of Brazil (Fig. 1). Firstly, visual classification of all the boards was done, to select 60 boards free of defects (knots or cracks). The moisture content of boards at the time of the tests was close 12%, according to ABNT NBR 7190:1997 [23]. The 60 boards were weighed and measured using caliper (in the cross-section) and tape (length - axial direction to the grain).



Fig. 1. Batch of *Schizolobium amazonicum* Herb

2.2 Modulus of Elasticity in Static Bending

For wood modulus of elasticity determination by three points static bending (MOE_{sb}), the rupture (F_{rup}) of a specimen was estimated. After that, were determined at 10% ($F_{10\%}$) and 50% ($F_{50\%}$) of the rupture the respective deflections ($v_{10\%}$; $v_{50\%}$) for all 60 boards (Fig. 2). These percentages were selected according to ABNT NBR 7190:1997 [23] because it ensures that the elastic regime of wood has not been exceeded. For the calculation of MOE_{sb} , Equation (1) was used, where L is the length between supports, and b and h are the cross-section width and thickness, respectively.

$$MOE_{sb} = \frac{(F_{50\%} - F_{10\%}) \cdot L^3}{(v_{50\%} - v_{10\%}) \cdot 4 \cdot b \cdot h^3} \quad (1)$$

2.3 Modulus of Elasticity in Longitudinal Vibration

Modulus of elasticity in longitudinal vibration (MOE_{lv}) was determined by the Equation (2), where ρ_{ap} is the wood density, l is the board length and f is the longitudinal vibration frequency.

$$MOE_{lv} = \rho_{ap} \cdot (2 \cdot l \cdot f)^2 \quad (2)$$

Boards were placed on two supports, on one side was placed a microphone to capture the longitudinal vibration frequency and the other free (Fig. 3), for impact with hammer, according to the methodology proposed by Fakopp Enterprise [35], which also provides the software for determination of vibration frequency based on the Fast Fourier Vibration Analyzer.

2.4 Density

Wood density (ρ_{ap}) was determined according to ABNT NBR 7190:1997 [23] through the Equation (3), where m and V are weight and volume of the specimen, respectively.

$$\rho_{ap} = \frac{m}{V} \quad (3)$$



(a)



(b)

Fig. 2. Static bending test: (a) board in test; (b) instrumenting details.

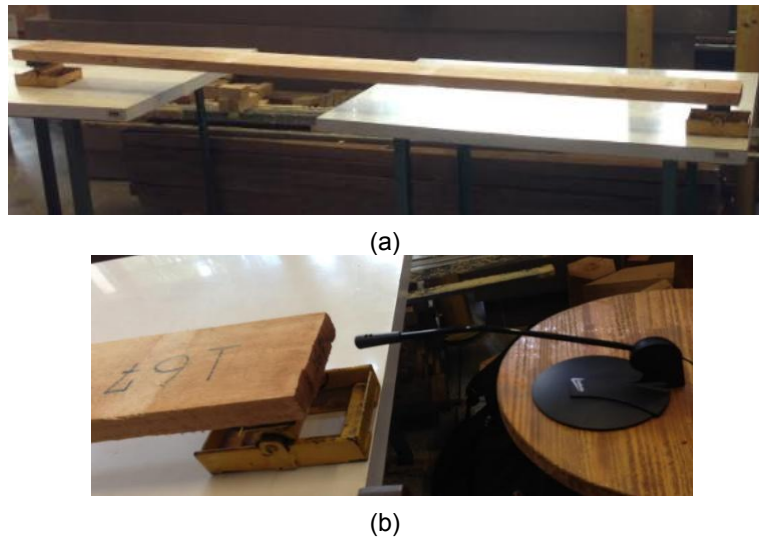


Fig. 3. Longitudinal vibration test: (a) board in test; (b) microphone close to the board.

2.5 Statistical Analysis and Regression Models

Statistical analysis and the proposed regression models were performed using the software R version 3.4.2 [36]. Polynomial univariate regression models of degrees 1 and 2 were tested with the aid of analysis of variance (ANOVA), with MOE_{iv} being the independent variable, and MOE_{sb} the dependent variable, of the functions adjusted by the least squares method.

Also, through ANOVA, a multivariate regression model was tested with the purpose of using the densities of the wood pieces (together with the modulus of elasticity determined by sound), considering the influence of density on the mechanical properties of wood [37] as an explanatory variable, adjusted by least squares method.

For the regression model's ANOVA, also evaluated at the 5% significance level, the stipulated null hypothesis consisted in the non-representativeness of the tested models ($H_0: \sigma=0$), and representativeness as an alternative hypothesis ($H_1: \sigma \neq 0$). P-value higher than the level of significance considered implies accepting H_0 , refuting it otherwise.

In addition to ANOVA, which allows to accept the representativeness of tested models, the adjusted coefficient of determination (R^2) values were obtained as a way of evaluating the capacity of the variations of the independent variable X to explain the predictive variable Y,

among the models, considered significant, the one of best fit by tested relation.

3. RESULTS AND DISCUSSIONS

3.1 Properties of Schizolobium Amazonicum Herb. Wood

Table 1 shows the average (x_m), maximum (Max) and minimum (Min) of modulus of elasticity values obtained by the methods of longitudinal vibration and static bending and the density of the *Schizolobium amazonicum* Herb. boards. Besides, the coefficient of variation (CV) determined for each property studied are also presented. The average value of MOE_{iv} is higher than the average value of MOE_{sb} , both values were higher than those determined by Cavalheiro et al. [38].

Table 1. Modulus of elasticity and density of *Schizolobium amazonicum* Herb.

Properties	x_m	CV (%)	Min	Max
MOE_{sb} (GPa)	9.07	20.52	5.51	12.86
MOE_{iv} (GPa)	9.70	19.72	5.39	12.7
ρ_{ap} (kg/m ³)	381.21	13.13	238.33	474.21

Almeida et al. [39] found the modulus of elasticity average value of *Schizolobium amazonicum* Herb. by transverse vibration technique equal to 7.75 GPa, lower than the average values determined in this research.

Almeida et al. [40] studied the complete characterization of *Schizolobium amazonicum* Herb. wood in structural dimensions pieces and

found a modulus of elasticity in static bending average value equal to 8.90 GPa, lower than that determined for the batch of this research.

The studied batch of *Schizolobium amazonicum* Herb. presented density equal 381.21 kg/m³, lower than that determined by Terezo and Szücs [20], which reached an average density equal to 490 kg/m³.

Differences between average values found for modulus of elasticity and density are explained by the fact that wood is a material of natural origin and it is influenced by several factors, including anatomical and biotic ones [41,42].

3.2 Regression Models

Figures 3 and 4 present the graphs of linear and quadratic regression models for estimation of MOE_{sb} as a function of MOE_{lv}, respectively. Linear and quadratic regression models presented coefficients of determination equal to 61.80 and 62.65% (Fig. 4 and Fig. 5), respectively. Multivariate linear regression model for MOE_{sb} estimation as a function of MOE_{lv} and density (Equation 4) showed a coefficient of determination equal to 61.27%. The coefficient of determination values found for correlations proposed in this study was satisfactory for estimation of MOE_{sb}.

$$MOE_{sb} = 1.211403 + 0.723266 MOE_{lv} + 0.002212 \cdot \rho_{ap} \quad (4)$$

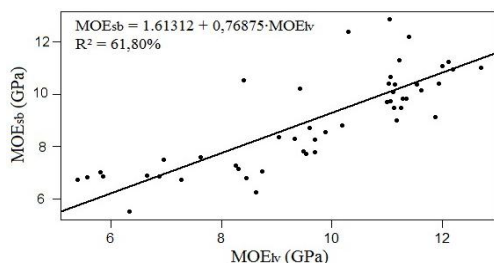


Fig. 4. Linear regression model for MOE_{sb} as a function of MOE_{lv}.

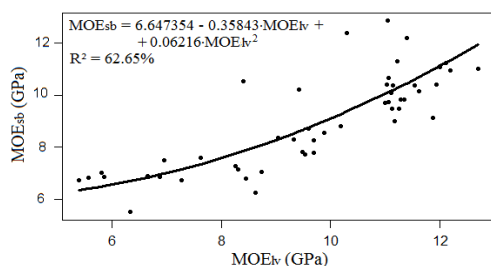


Fig. 5. Quadratic regression model for MOE_{sb} as a function of MOE_{lv}.

Tables 2, 3 and 4 present the statistics DF (Degree freedom), SS (Sum Square), MS (Multiple Square), F-value and P-value for the factors used for linear, quadratic and multivariate linear regression models, respectively. The influence of density on the multivariate linear regression model was not significant (P-value = 0.652), as well as the quadratic parcel of the quadratic model (P-value = 0.134).

Table 2. Linear regression model statistics

Source	DF	SS	MS	F-value	P-value
MOE _{lv}	1	127.80	127.80	96.46	0.000
Residuals	58	76.84	1.33	-	-
Total	59	204.65	-	-	-

Table 3. Quadratic regression model statistics

Source	DF	SS	MS	F-value	P-value
MOE _{lv}	1	127.80	127.80	98.65	0.000
MOE _{lv} ²	1	3.00	3.00	2.31	0.134
Residuals	57	73.85	1.30	-	-
Total	59	204.65	132.10	-	-

Table 4. Multivariate linear regression model statistics

Source	DF	SS	MS	F-value	P-value
MOE _{lv}	1	127.80	127.80	95.14	0.00
ρ _{ap}	1	0.28	0.28	0.21	0.652
Residuals	57	76.57	1.34	-	-
Total	59	204.65	129.42	-	-

Chen and Guo [43] performed a linear correlation for MOE in static bending as a function of MOE in stress wave technique to *Abies fabri* (Mast.) Craib wood, finding coefficient of determination value equal to 63.50%.

Martins et al. [44] conducted research using *Pinus pinaster* (Ait.) poles. A linear regression model was adopted for estimation of mechanical MOE as a function of modulus of elasticity by the longitudinal vibration technique. The coefficient of determination, in this case, was equal to 31%.

Chen and Guo [45] estimated the modulus of elasticity of *Cunninghamia lanceolata* Lamb. Hook and *Ulmus rubra* wood by the techniques of static bending and stress wave. Coefficients of determination of linear regression models proposed for estimation of MOE in static bending as a function of stress wave MOE were equal to 50.20% and 63.30% for *Cunninghamia lanceolata* Lamb. Hook and *Ulmus rubra* wood, respectively.

Oberhofnerová et al. [46] carried out tests to estimate the modulus of elasticity in static bending and longitudinal vibration for *Picea abies* and *Quercus robur* wood and the coefficient of determination values for linear correlations were 50.58% and 47.33%, respectively.

4. CONCLUSIONS

According to the discussion of the obtained results, the values of modulus of elasticity in longitudinal vibration and in static bending estimated for the batch of *Schizolobium amazonicum* Herb. studied in this research presented average values of 9.70 and 9.07 GPa, and density equal to 381.21 kg/m³. Regression models proposed for estimation of MOE_{sb} presented coefficient of determination values close to 60%.

COMPETING INTERESTS

Authors have declared that no competing interests exist.

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